reduction and annealing, each of the aforementioned lead alloys was tested for hardness. A minimum of six hardness measurements at each of two locations of the test alloys were obtained using a Shimadzu model HMV2000 micro hardness tester utilizing a 25g load. The hardness of each metal was also measured in the same way in the as-cast condition (i.e. without being subjected to deformation and annealing cycle). The f_{sp} count of the as-cast material samples prior to GBE processing in all cases was between 10 and 15%. The results of the hardness test for each of the lead alloys is shown in Table 2. In all instances, the deformation reduction and heat annealing cycle(s) resulted in an alloy having a lower hardness than the one of the corresponding as-cast alloy.--

Please replace the paragraph on page 30, beginning with the term "EXAMPLE #11" at line 9, and ending on page 30, line 17 (as amended in the amendment dated March 25, 2002), with the following rewritten paragraph:

--EXAMPLE #11:

Two Pb-Ca-Sn alloys were cast into sheets. An as received set representing prior art and a set processed according to the invention were corrosion tested in an environment representative of a zinc-electrowinning operation. The peening was performed using 28 mil steel shot at 80 psi at room temperature. Three passes per substrate were performed within three minutes and the peened samples were subsequently annealed at 250 °C for 10 minutes. A pretreatment comprising a 30 minute soak at 300 °C was used to modify existing precipitates to facilitate the GBE process. The following tables 9 and 10 illustrate the sample characteristics and the corrosion performance.--

Serial No. 09/991,702

Please replace the paragraph on page 21, beginning at line 14 and ending on page 21, line 19, with the following rewritten paragraph:

A Pb-0.073wt% Ca-0.7 wt% Sn alloy (Class II) was processed by three cycles each comprised of cold rolling at room temperature to achieve a 40% reduction in thickness, annealing at 270 °C for 10 minutes in air followed by air cooling. The resulting microstructural improvement in terms of special grain boundary content is summarized in Figure 5 (identified as PbCaSn in Figure 5). The special grain boundary content was increased from 11% in the as-cast starting material, to 51% in the material processed by the method described.

Please replace the paragraph on page 21, beginning at line 21 and ending on page 21, line 26, with the following rewritten paragraph:

A Pb-0.065wt% Ca-0.7 wt% Sn 0.03wt% Ag alloy (Class II) was processed by two cycles each comprised of cold rolling at room temperature to achieve a 40% reduction in thickness, annealing at 250 °C for 10 minutes in air followed by air cooling. The resulting microstructural improvement in terms of special grain boundary content is summarized in Figure 5 (identified as PbCaSnAg in Figure 5). The special grain boundary content was increased from 12% in the as-cast starting material, to 70% in the material processed by the method described.